ARLINGTON AVENUE MIXED-USE PRELIMINARY DRAINAGE STATEMENT





05/22/23

Project Title: Arlington Mixed- Use Project Address: 5261 Arlington Avenue, Riverside

Prepared for:

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1.0 Introduction

1.1 Project Description

Foulger- Pratt proposes to demolish an existing retail department building and at grade parking lot and construct 388 residential units across 27 buildings with a leasing office, new grocery store, and a retail unit with on-site at-grade parking, drive aisles, amenities, and landscape withing a 17.43-acre site. The site is located at the northeast corner of the Arlington Avenue and Streeter Avenue. The approximate area after the dedication is 17.37-acres.

1.1 Purpose of the Study

The purpose of this drainage statement is to describe the existing and proposed conditions, and how the proposed drainage improvements comply with the City of Riverside and the Riverside County Flood Control and Water Conservation District requirements.

2.0 Pre- Development Condition Hydrology

2.1 Pre-Development Condition Hydrology

The project is tributary to the Santa Ana River, Reach 3. Under existing conditions, the entire project parcel (17.47 acres) slopes to the west. The lot drains into two existing 30" storm drains and one existing 33" storm drain within Streeter Avenue. From there, the stormwater collected in the municipally maintained stormwater system discharges into a flood control channel.

2.2 Methodology of Hydrology Study

Per the Riverside County Hydrology Design Manual, the 10-yr storm event will be considered the design storm for this project. The 100-yr pre-development peak flow has also been calculated and provided for additional data. The Riverside County Hydrology Design Manual uses the Rational Method for calculation of the pre-development peak discharges. The Rational Method (Q=CIA) calculates the discharge (Q) based on the runoff coefficient ©, rainfall intensity (I) and the area of the watersheds (A) within the project. The runoff coefficient for the existing site was calculated per standard "Urban Landscaping" "C" curves, Plates D-5.3. The rainfall intensity (I) was calculated using the standard Riverside area plate D-4. The project site has been evaluated as the following three drainage areas: EX-1, EX-2, and EX-3. The drainage area EX-2 includes the offsite runoff from the east. The drainage area of that runoff is O1.

2.3 Hydrology Calculations

The resulting 10-year pre-development peak discharges are summarized in **Table 1** below. In these calculations, there was an adjustment for the peak flow at the junction. Since the tributary areas have different times of concentration, the smaller tributary flows were corrected. Point 1 and Point 3 were corrected with the adjustment.

ARLINGTON AVENUE MIXED-USE PRELIMINARYDRAINAGE STATEMENT

		Tal	ble 1					
Drainage Area	Soil Group	Development	Area (sf)	Area (acre)	l10 (in/hr)	С	ণ্ট Q (ft ³ /s)	♦ Q10 (ft ³ /s)
EX-1A	В	Commercial	94,023	2.16	2.23	0.9	4.33	4.33
EX-1B	В	Commercial	207,600	4.77	1.90	0.90	8.15	12.48
TOTAL - Point 1				6.92				8.14
Drainage Area	Soil Group	Development	Area (sf)	Area (acre)	l10 (in/hr)	с	♥ Q (ft ³ /s)	♦ Q10 (ft ³ /s)
01	В	Commercial	29,058	0.67	1.90	0.8	1.01	1.01
EX-2A	В	Commercial	58,296	1.34	1.40	0.9	1.69	2.70
EX-2B + EX-2C	В	Commercial	301,203	6.91	1.24	0.9	7.72	10.42
TOTAL - Point 2				8.92				10.42
Drainage Area	Soil Group	Development	Area (sf)	Area (acre)	l10 (in/hr)	с	ণ্ণ Q (ft ³ /s)	♦ Q10 (ft ³ /s)
EX-3A	В	Commercial	97,888	2.25	2.07	0.9	4.19	4.19
-	В	Commercial	-	2.25	1.97	0.9	3.99	3.99
TOTAL - Point 3				2.25				2.51

Table 1

2.4 Results of Pre- Development Hydrology Calculations

In these calculations, there was an adjustment for the peak flow at the junction. Since the tributary areas have different times of concentration, the smaller tributary flows were corrected. Point 1 and Point 3 were corrected with the adjustment. Please refer to **Appendix 1** for the pre-developed 10-year and 100-year calculations with adjustments. The combined pre-development 10-year peak discharge (Q_{10}) for the site results in 21.07cfs. Similarly, the combined pre- development 100-year peak discharge (Q_{100}) for the site results in 31.31cfs.

3.0 Post- Development Conditions

3.1 Post-Development Condition Hydrology

This project proposes to construct 27 buildings with a total of 388 residential units, a leasing office, new grocery store, and a retail unit with at-grade parking, drive aisles, amenities, and landscaping on a 17.37-acre site in the City of Riverside. The proposed condition incorporates stormwater runoff from Granada Avenue to the east. Due to the proposed site design, the computations for sizing the on- site storm drain system and water quality treatment devices there as a total of 8 Drainage Management Area (DMAs) with three discharge locations. Stormwater from Granada Avenue (O1) is conveyed through the site but bypasses the LID treatment devices. The north side of the site discharges to an existing 30" storm drain (Point 1), the middle of the site discharges to an existing 33" storm drain (Point 3) within Streeter Avenue. The stormwater collected then discharges into a flood control channel.

3.2 Methodology of Hydrology Study

The 10-yr peak discharge generated onsite was calculated using the Rational Method. The resulting 10-yr peak discharge has been summarized in **Table 2** below.

		1 a	ble 2					
Drainage Area	Soil Group	Development	Area (sf)	Area (acre)	l (in/hr)	С	ণ্ণ Q (ft ³ /s)	♦ Q10 (ft ³ /s)
PR-1A	В	Apartment	10,482	0.24	2.42	0.8	0.47	0.47
PR-1B	В	Apartment	111,748	2.57	1.65	0.8	3.39	3.85
-	-	-	0	0.00	1.60	0	0.00	3.85
TOTAL- Point 1				2.81				2.79
Drainage Area	Soil Group	Development	Area (sf)	Area (acre)	l (in/hr)	С	ণ্ণ Q (ft ³ /s)	♦ Q10 (ft ³ /s)
PR-2A	В	Apartment	10,466	0.24	2.09	0.8	0.40	0.40
PR-2B	В	Apartment	113,984	2.62	1.81	0.8	3.79	4.19
01	В	Commercial	29,058	0.67	1.79	0.89	1.06	1.06
PR-2C	В	Apartment	199,674	4.58	1.28	0.8	4.69	9.95
PR-2D	В	Apartment	93,221	2.14	1.17	0.8	2.00	11.95
-	В	-	0	0.00	1.16	0	0.00	11.95
TOTAL- Point 2				10.25				11.95
Drainage Area	Soil Group	Development	Area (sf)	Area (acre)	l (in/hr)	С	্ষ Q (ft ³ /s)	♦ Q10 (ft ³ /s)
PR-3A	В	Apartment	13,490	0.31	2.32	0.8	0.57	0.57
PR-3B	В	Apartment	111,609	2.56	1.82	0.8	3.73	4.31
-	В	-	0	0.00	1.67	0	0.00	4.31
TOTAL- Point 3				2.87				2.99

Table 2

3.4 Results of Post- Development Hydrology Calculations

In these calculations, there was an adjustment for the peak flow at the junction. Since the tributary areas have different times of concentration, the smaller tributary flows were corrected. Point 1 and Point 3 were corrected with the adjustment. Please refer to **Appendix 2** for the post-developed 10-year and 100-year calculations with adjustments. The combined post- development Q_{10} for the site results in 17.73cfs. Similarly, the combined post- development Q_{100} for the site results in 25.45cfs.

4.0 Comparison of Post- Development and Pre- Development Hydrologic Conditions

ARLINGTON AVENUE MIXED-USE PRELIMINARYDRAINAGE STATEMENT

4.1 Hydrologic Calculations Methodology

The site is in an area of a Hydrologic Condition of Concern. Therefore, a 2-year storm event was considered. RRIV¹ and Hydrographs² software packages were used to route the storm drain system and find the 2- year peak discharge (Q_2). The Q_2 at the point of compliance will generate 18.58cfs in the pre-developed condition. The Q_2 at the point of compliance will generate 16.44cfs in the post-developed condition. This results in a 2.14cfs reduction. This is due to the decrease in imperviousness area from 99% to approximately 72%. While the final impervious area will depend on the final design, a significant reduction of imperviousness generally decreases the peak discharge. Please see **Appendix 3** for the calculations.

5.0 Hydraulic Calculations

5.1 Hydraulic Calculations Methodology

The drainage from the building roofs and interior roadways will be collected through roof drains, site are drains, and catch basins. The site's storm drain system will then route the collected stormwater though the proposed storm drain system into the corresponding modular wetland BMP for biotreatment before it is discharges into the flood control channel on Streeter Avenue. The storm drain system has been preliminary sized using the Rational Method as listed as an acceptable method within the Riverside County Hydrology Manual. Please refer to **Appendix 2** which includes the preliminary pipe size and slope. The final pipe sizing will be analyzed to verify the hydraulic grade line (HGL) based on the 10-year storm event peak flow rates and a summary table will be provided to substantiate sizes during final engineering for the post- development onsite conveyance pipe. Catch basin sizing will also be analyzed and a summary table will be provided to substantiate the size during final engineering.

6.0 Conclusion

The storm drain system has been sized according to the Riverside Country Hydrology Manual by using the Rational Method. The proposed storm drain sizing throughout the site meets the design requirements for capture of the flow generated from the 10-yr storm event, meeting the City of Riverside requirements.

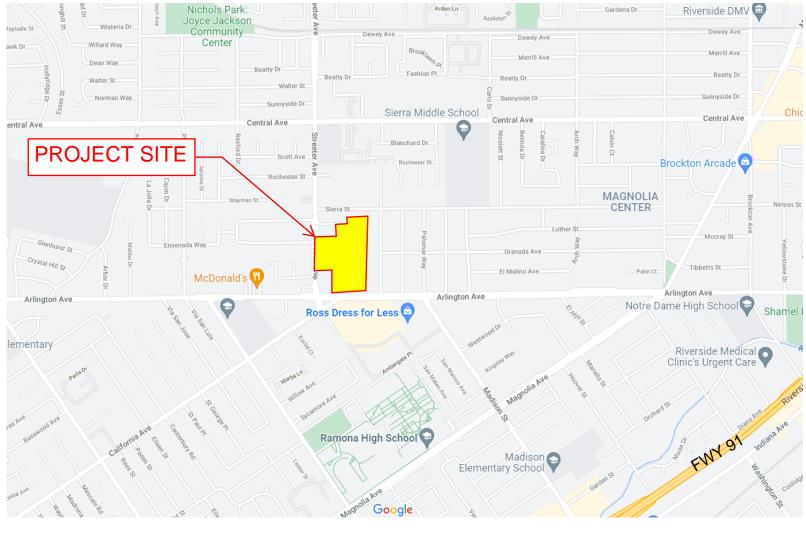
The overall site will generate a peak runoff for a 10-year event of 17.73cfs. The pre-developed site generates a peak runoff of 21.07cfs. The post- development peak runoff has been reduced from the pre- development condition. Therefore, the project will not have an adverse downstream effect or require offsite storm drain mitigation.

¹ PRIV: Rational Hydrology Method, Riverside County developed by CivilDesign is a widely available and accepted software package for preparing hydrology calculations based on the Riverside County Flood Control and Water Conservation District, Hydrology Manual.

² Hydrographs is a software application that is part of the Autodesk Civil 3D suite. It allows users to perform a variety of storm water management tasks, including hydrologic analysis and hydraulic modeling of watersheds.

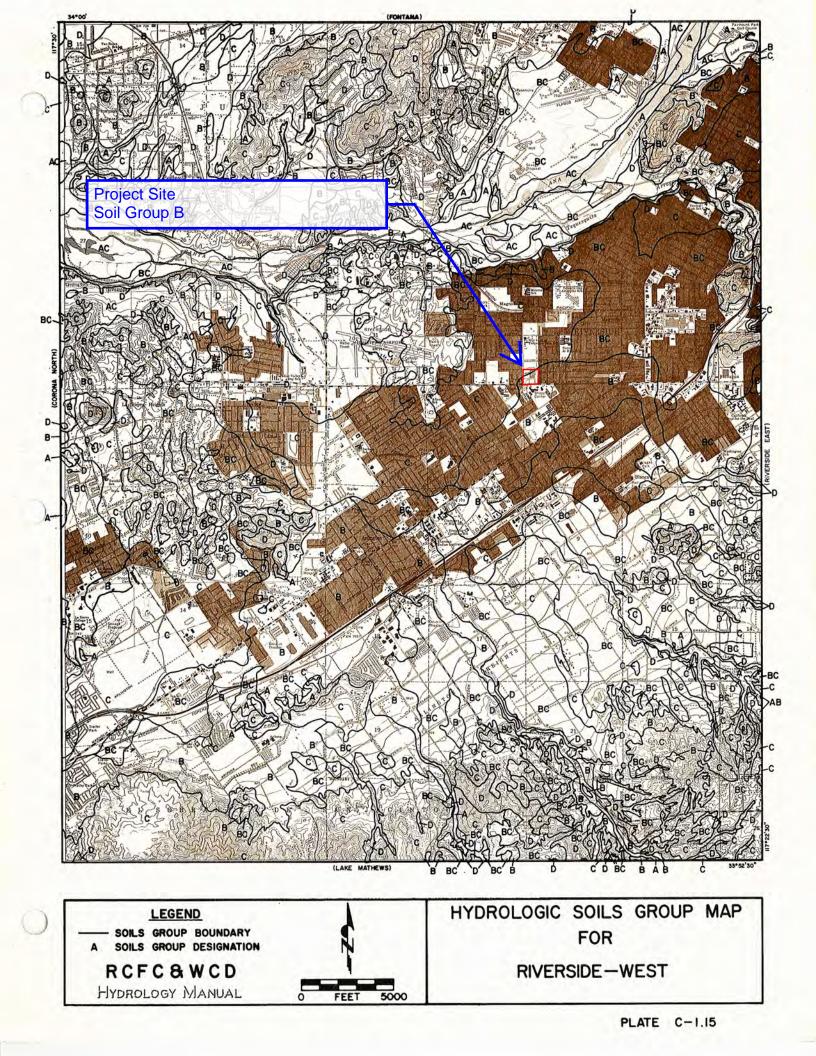
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7.0 Exhibits Exhibit A: Location Map



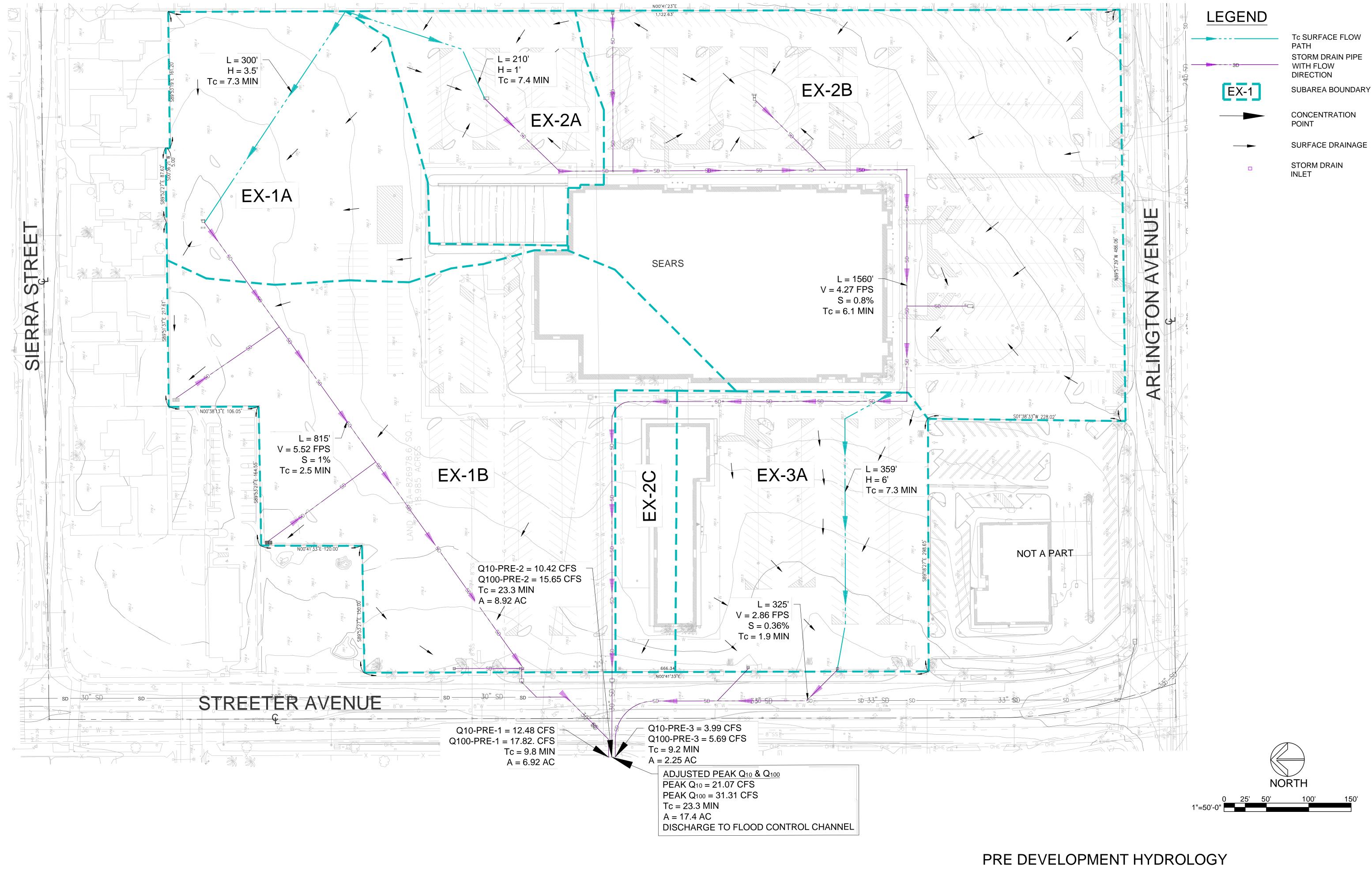
PROJECT LOCATION MAP

Exhibit B: Hydrologic Soil Group Map



ARLINGTON AVENUE MIXED-USE PRELIMINARYDRAINAGE STATEMENT

Exhibit C: Pre- Development Hydrology Map





RIVERSIDE, CA



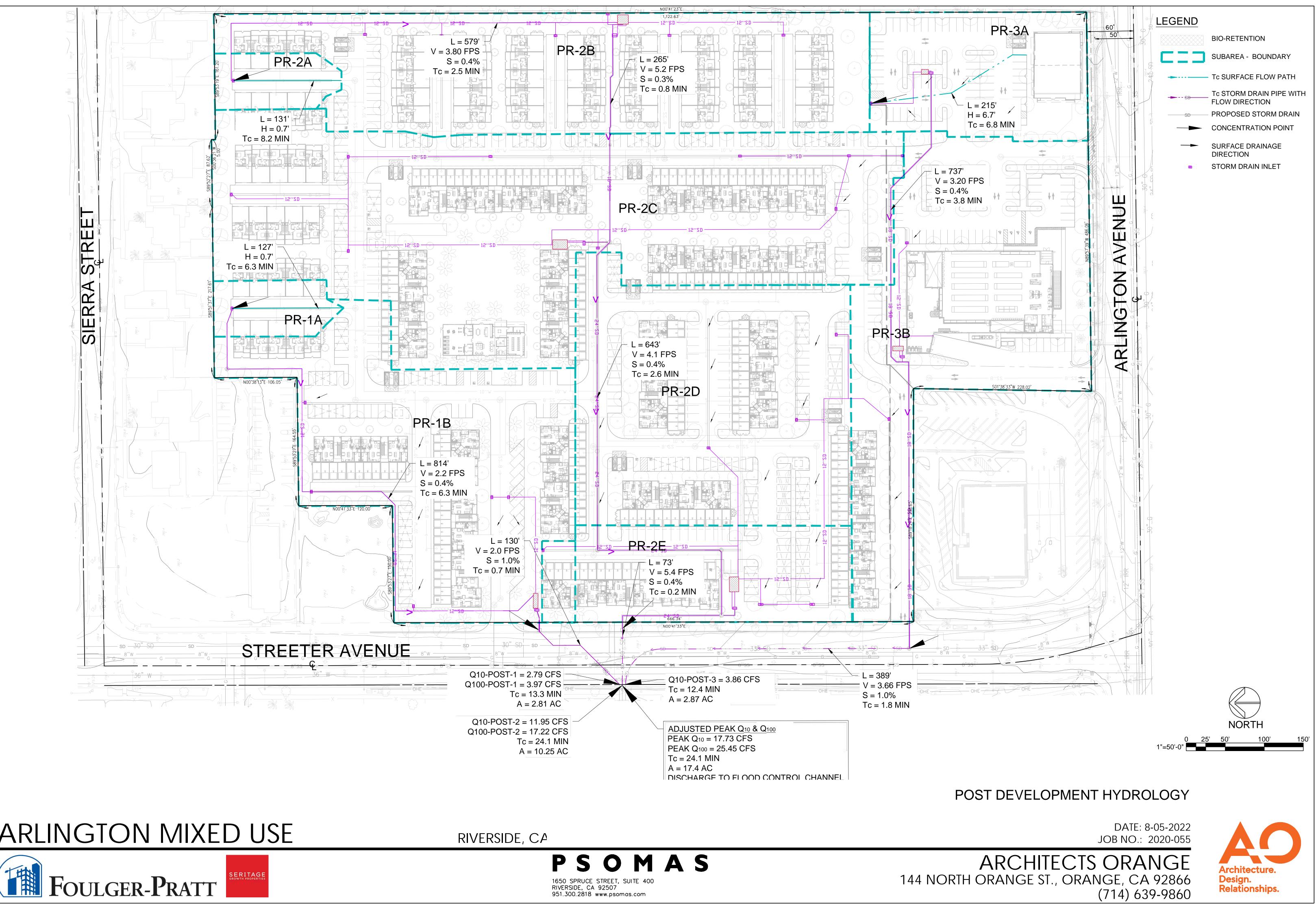


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Exhibit D: Post- Development Hydrology Map











7.0 Appendices

Appendix 1: Pre-Development Hydrology Calculations

Riverside County Pre Development Flow Calculations

Project: Arlington Mixed Use, Riverside, CA

Riverside County Flood Control and Water Conservation District Hydrology Rational Method Calculation Form

Condition:	Pre Dev	velopment
Frequency:	10-yr	
Calculated By:	NT	4/24/2023

Drainage Area	Soil Group	Development	Area (sf)	Area (acre)	l10 (in/hr)	с	♥ Q (ft³/s)	♦ Q10 (ft ³ /s)	Slope	Section	V (ft/s)	L (ft)	ণ্ণ H (ft)	T (min)	♦ T (min)	Remarks
EX-1A	В	Commercial	94,023	2.16	2.23	0.9	4.33	4.33	-	-	-	300	3.5	7.3	7.3	H = 9'; Initial Area (Plate D-3)
EX-1B	В	Commercial	207,600	4.77	1.90	0.90	8.15	12.48	0.010	30" Conc Pipe	5.52	815	8.000	2.5	9.8	Assume 18" @ 1% Conc Pipe
					Adjust Q	to Tc = 2	3.3 min.									
TOTAL - Point 1				6.92				8.14							23.3	Peak Q at Tp = 23.3 min.

Drainage Area	Soil Group	Development	Area (sf)	Area (acre)	l10 (in/hr)	с	♥ Q (ft ³ /s)	♦ Q10 (ft ³ /s)	Slope	Section	V (ft/s)	L (ft)	থ H (ft)	T (min)	♦ T (min)	Remarks
01	В	Commercial	29,058	0.67	1.90	0.8	1.01	1.01	-	-	-	150	0.5	9.8	9.8	
EX-2A	В	Commercial	58,296	1.34	1.40	0.9	1.69	2.70	-	-	-	210	1.0	7.4	17.2	Initial Area (Plate D-3)
EX-2B + EX-2C	В	Commercial	301,203	6.91	1.24	0.9	7.72	10.42	0.008	30" Conc Pipe	4.27	1560	12.5	6.1	23.3	Assume 18" @ 0.8% Conc Pipe
TOTAL - Point 2				8.92				10.42							23.3	Peak Q at Tp = 23.3 min.

Drainage Area	Soil Group	Development	Area (sf)	Area (acre)	l10 (in/hr)	с	৭ Q (ft ³ /s)	♦ Q10 (ft ³ /s)	Slope	Section	V (ft/s)	L (ft)	ণ্ণ H (ft)	T (min)	♦ T (min)	Remarks
EX-3A	В	Commercial	97,888	2.25	2.07	0.9	4.19	4.19	÷	-	-	359	6.0	7.3	7.3	Initial Area (Plate D-3)
-	В	Commercial	-	2.25	1.97	0.9	3.99	3.99	0.0036	33" Conc Pipe	2.86	325	-	1.9	9.2	33" RCP @ 0.36% Conc Pipe
					Adjust Q	to Tc = 2	3.3 min.									
TOTAL - Point 3				2.25				2.51							23.3	Peak Q at Tp = 23.3 min.

Notes

1 Intensity data per standard Riverside area (Plate D-4.1)

2 Runoff coefficient per standard "Urban Landscaping" "C" curves (Plates D-5.3)

3 Site is located entirely within Soil Group BC as classified by USFS. For the purpose of Hydrology analysis, Soil Group B is used as the more conservative approach.

ADJUSTMENTS TO POINT 1

		ENT DISCHARGE FROM SITE =	
TOTAL DISCHAR	GE FRO	M SITE = 8.14 + 10.42 + 2.51	
QADJUSTED =	2.51	cfs	
QADJUSTED =	3.99 x (1.2	24 / 1.97)	
I _B =	1.97	in/hr (intensity at Tc = 9.2 min)	
IA =	1.24	in/hr (intensity at Tc = 23.3 min)	
QB =	3.99	cfs (Flow at Tc = 9.2 min)	
Adjust TB to TA =	23.3	min	
ADJUSTMENTS TO PO	DINT 3		
QADJUSTED =	8.14	cfs	
QADJUSTED =	12.48 x (1	.24 / 1.9)	
I _B =	1.90	in/hr (intensity at Tc = 9.8 min)	
IA =	1.24	in/hr (intensity at Tc = 23.3 min)	
QB =	12.48	cfs (Flow at Tc = 9.8 min)	
Adjust TB to TA =	23.3	min	

Riverside County Pre Development Flow Calculations

Riverside County Flood Control and Water Conservation District Hydrology Rational Method Calculation Form

Condition:	Pre Deve	elopment
Frequency:	100-yr	
Calculated By:	NT	4/24/2023

Project: Arlingt	on Mixed Use,	Riverside, CA
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Drainage Area	Soil Group	Development	Area (sf)	Area (acre)	1100 (in/hr)	С	♥Q (ft³/s)	♦ Q100 (ft ³ /s)	Slope	Section	V (ft/s)	L (ft)	ণ্ণ H (ft)	T (min)	♦ T (min)	Remarks
EX-1A	В	Commercial	94,023	2.16	3.19	0.9	6.20	6.20	-	-	-	300	3.5	7.3	7.3	H = 9'; Initial Area (Plate D-3)
EX-1B	В	Commercial	207,600	4.77	2.71	0.90	11.62	17.82	0.010	30" Conc Pipe	5.520	8.150	8.000	2.5	9.8	Assume 18" @ 1% Conc Pipe
					Adjust Q	to Tc = 23	3.3 min.									
TOTAL - Point 1				6.92				11.97							23.3	Peak Q at Tp = 23.3 min.

Drainage Area	Soil Group	Development	Area (sf)	Area (acre)	1100 (in/hr)	с	♥ Q (ft³/s)	♦ Q100 (ft ³ /s)	Slope	Section	V (ft/s)	L (ft)	ণ H (ft)	T (min)	♦ T (min)	Remarks
01	В	Commercial	29,058	0.67	2.99	0.9	1.80	1.80				150	0.5	9.8	9.8	
EX-2A	В	Commercial	58,296	1.34	2.10	0.9	2.53	4.32	-	-	-	210	1.0	7.4	17.2	Initial Area (Plate D-3)
EX-2B + EX-2C	В	Commercial	301,203	6.91	1.82	0.9	11.33	15.65	0.008	30" Conc Pipe	4.27	1560	12.5	6.1	23.3	Assume 18" @ 0.8% Conc Pipe
TOTAL - Point 2				8.92				15.65							23.3	Peak Q at Tp = 23.3 min.

Drainage Area	Soil Group	Development	Area (sf)	Area (acre)	l100 (in/hr)	с	৭ Q (ft ³ /s)	♦ Q100 (ft ³ /s)	Slope	Section	V (ft/s)	L (ft)	ণ্ণ H (ft)	T (min)	♦ T (min)	Remarks
EX-3A	В	Commercial	97,888	2.25	3.19	0.9	6.45	6.45	-	-	-	359	6.0	7.3	7.3	Initial Area (Plate D-3)
-	В	Commercial	-	2.25	2.81	0.9	5.69	5.69	0.0036	33" Conc Pipe	2.86	325	-	1.9	9.2	33" RCP @ 0.36% Conc Pipe
					Adjust Q	to Tc = 2	3.3 min.									
TOTAL - Point 3				2.25				3.69							23.3	Peak Q at Tp = 23.3 min.

Notes

1 Intensity data per standard Riverside area (Plate D-4.1)

2 Runoff coefficient per standard "Urban Landscaping" "C" curves (Plates D-5.3)

3 Site is located entirely within Soil Group BC as classified by USFS. For the purpose of Hydrology analysis, Soil Group B is used as the more conservative approach.

ADJUSTMENTS TO POINT 1

TOTAL PRE-DEVE	LOPME	NT DISCHARGE FROM SITE =	31.31 CFS @ Tc = 23.3 MIN
TOTAL DISCHAR	ge froi	M SITE = 11.97 + 15.65 + 3.69	
QADJUSTED =	3.69	cfs	
QADJUSTED = 5	5.69 x (1.8	2 / 2.81)	
Ів =	2.81	in/hr (intensity at Tc = 9.2 min)	
IA =	1.82	in/hr (intensity at Tc = 23.3 min)	
QB =	5.69	cfs (Flow at Tc = 9.2 min)	
Adjust TB to TA =	23.3	min	
ADJUSTMENTS TO PC	DINT 3		
QADJUSTED =	11.97	cfs	
QADJUSTED = 1	L7.82 x (1	.82 / 2.71)	
18 -	2.71		
Iв =	2.71	in/hr (intensity at Tc = 9.8 min)	
IA =	1.82	in/hr (intensity at Tc = 23.3 min)	
Qв =	17.82	cfs (Flow at Tc = 9.8 min)	
Adjust TB to TA =	23.3	min	

ARLINGTON AVENUE MIXED-USE PRELIMINARYDRAINAGE STATEMENT

Appendix 2: Post-Development Hydrology Calculations

Riverside County Post Development Flow Calculations

Riverside County Flood Control and Water Conservation District Hydrology Rational Method Calculation Form

Rational Method Ca	Iculation Form	CA	istrict Hydroit	2 57														Conditio Frequen Calculat	cy:		Post De 10-yr NT	evelopment 4/27/2023
Drainage Area	Soil Group	Development	Area (sf)	Area (acre)	l (in/hr)	с	♥ Q (ft³/s)	♦ Q10 (ft ³ /s)	Slope	Section (P Dia.)	ipe Manning's (n)	Vf (ft/s)	Qf	Q/Qf	d/D	V/Vf	V (ft/s)	L (ft)	ч н (ft)	T (min)	♦T (min)	Remarks
PR-1A	В	Apartment	10,482	0.24	2.42	0.8	0.47	0.47		-	-	-	-	-	-	-	-	127	0.7	6.3	6.3	Initial Area (Plate D-3)
PR-1B	В	Apartment	111,748	2.57	1.65	0.8	3.39	3.85	0.004	15.0	0.012	3.617	4.44	86.8%	0.7	1.1	2.2	815	-	6.3	12.6	
-	-	-	0	0.00	1.60	0	0.00	3.85	0.010	30.0	0.012	9.077	44.56	8.6%	0.2	0.6	2.0	130	-	0.7	13.3	At Flood Control Basin
TOTAL- Point 1				2.81				2.79													24.1	Peak Q at Tp = 24.1 min.
Drainage Area	Soil Group	Development	Area (sf)	Area (acre)	l (in/hr)	с	♥ Q (ft ³ /s)	♦ Q10 (ft ³ /s)	Slope	Section	Manning's (n)	Vf (ft/s)	Qf	Q/Qf	d/D	v/vf	V (ft/s)	L (ft)	Ф Н (ft)	T (min)	♦ T (min)	Remarks
PR-2A	В	Apartment	10,466	0.24	2.09	0.8	0.40	0.40	-	-	-	-		-	-	-	-	131	0.7	8.2	8.2	Initial Area (Plate D-3)
PR-2B	В	Apartment	113,984	2.62	1.81	0.8	3.79	4.19	0.004	15.0	0.012	3.617	4.44	94.4%	0.8	1.1	3.8	579	-	2.5	10.7	
01	В	Commercial	29,058	0.67	1.79	0.89	1.06	1.06	-		-						-	150	0.5	9.8	9.8	
PR-2C	В	Apartment	199,674	4.58	1.28	0.8	4.69	9.95	0.004	24.0	0.012	4.947	15.54	64.0%	0.6	1.1	5.2	265		0.8	21.3	
PR-2D	В	Apartment	93,221	2.14	1.17	0.8	2.00	11.95	0.004	24.0	0.012	4.947	15.54	76.9%	0.7	1.1	4.1	643	-	2.6	23.9	
	В		0	0.00	1.16	0	0.00	11.95	0.010	30.0	0.012	9.077	44.56	26.8%	0.4	0.9	5.4	73	-	0.2	24.1	At Flood Control Basin
TOTAL- Point 2				10.25				11.95													24.1	Peak Q at Tp = 24.1 min.
Drainage Area	Soil Group	Development	Area (sf)	Area (acre)	l (in/hr)	с	♥ Q (ft ³ /s)	♦ Q10 (ft ³ /s)	Slope	Section	Manning's (n)	Vf (ft/s)	Qf	Q/Qf	d/D	V/Vf	V (ft/s)	L (ft)	Ф Н (ft)	T (min)	♦T (min)	Remarks
PR-3A	В	Apartment	13,490	0.31	2.32	0.8	0.57	0.57	-	-	-	-	-	-	-	-	-	215	6.7	6.8	6.8	Initial Area (Plate D-3)
PR-3B	В	Apartment	111,609	2.56	1.82	0.8	3.73	4.31	0.004	18.0	0.012	4.084	7.22	59.7%	0.6	1.1	3.2	737	-	3.8	10.6	
-	В		0	0.00	1.67	0	0.00	4.31	0.010	33.0	0.012	9.672	57.45	7.5%	0.2	0.5	3.7	389	-	1.8	12.4	At Flood Control Basin
TOTAL- Point 3				2.87				2.99													24.1	Peak Q at Tp = 24.1 min.

ADJUSTMENTS TO POINT 1

5 ((F) (T (A A A))
5 cfs (Flow at Tc = 13.3 min)
6 in/hr (intensity at Tc = 24.1 min)
in/hr (intensity at Tc = 13.3 min)
(1.16/1.6)
9 cfs

ADJUSTMENTS TO POINT 3

Adjust TB to TA =	24.1	min						
QB =	4.31	cfs (Flow at Tc = 12.4 min)						
I _A =	1.16	in/hr (intensity at Tc = 24.1	min)					
In =	1.67	n/hr (intensity at Tc = 12.4 min)						
QADJUSTED =	4.31 x (1.1	6 / 1.67)						
QADJUSTED =	2.99	cfs						
TOTAL DISCHARGE FROM SITE = 2.79 + 11.95 + 2.99								
TOTAL POST-DE	TOTAL POST-DEVELOPMENT DISCHARGE FROM SITE = 17.73 CFS @ Tc = 24.1 MIN							

Riverside County Post Development Flow Calculations

Riverside County Flood Control and Water Conservation District Hydrology Rational Method Calculation Form

tional Method Ca	alculation Form			JEN														Conditio Frequen Calculate	cy:		100-yr	velopment 4/27/2023
Drainage Area	Soil Group	Development	Area (sf)	Area (acre)	l (in/hr)	с	♥ Q (ft ³ /s)	♦ Q100 (ft ³ /s)	Slope	Section (Pipe Dia.)	Manning's (n)	Vf (ft/s)	Qf	Q/Qf	d/D	V/Vf	V (ft/s)	L (ft)	ФН (ft)	T (min)	♦T (min)	Remarks
PR-1A	С	Apartment	10,482	0.24	3.46	0.8	0.67	0.67		-	-	-	-	-	-	-	-	127	0.7	6.3	6.3	Initial Area (Plate D-3)
PR-1B	C	Apartment	111,748	2.57	2.36	0.8	4.84	5.51	0.004	18.0	0.012	3.874	6.85	80.5%	0.7	1.1	2.2	794	-	6.3	12.6	
-	-		0	0.00	2.29	0	0.00	5.51	0.010	30.0	0.012	9.077	44.56	12.4%	0.2	0.6	2.0	130	-	0.7	13.3	At Flood Control Basin
					Adjust Q	to Tc = 2	4.1 min.															
TOTAL- Point 1				2.81	1		1	3.97													24.1	Peak Q at Tp = 24.1 min.
Drainage Area	Soil Group	Development	Area	Area	I	c		♦ Q100	Slope	Section	Manning's (n)	Vf	Of	Q/Qf	d/D	V/Vf	v	L	¶ H	т	¢т	Remarks
Diamage Area	Join Group	Development	(sf)	(acre)	(in/hr)	-	(ft ³ /s)	(ft ³ /s)	Slope	Jection	wanning 5 (ii)	(ft/s)	Q.	4/4/	4,5	•/•	(ft/s)	(ft)	(ft)	(min)	(min)	Kentarks
PR-2A	В	Apartment	10,466	0.24	2.97	0.8	0.57	0.57		-	-	-	-	-	-	-	-	131	0.7	8.2	8.2	Initial Area (Plate D-3)
PR-2B	В	Apartment	113,984	2.62	2.58	0.8	5.40	5.97	0.004	18.0	0.012	3.874	6.85	87.2%	0.7	1.1	3.8	579	-	2.5	10.7	
01	В	Commercial	29,058	0.67	2.71	0.89	1.61	1.61										150	0.5	9.8	9.8	
PR-2C	В	Apartment	199,674	4.58	1.82	0.8	6.67	14.25	0.004	24.0	0.012	4.947	15.54	91.7%	0.7	1.1	5.2	265	-	0.8	21.3	
PR-2D	В	Apartment	93,221	2.14	1.73	0.8	2.96	17.22	0.005	24.0	0.012	5.531	17.38	99.1%	0.8	1.2	4.1	643	-	2.6	23.9	
-	В	-	0	0.00	1.65	0	0.00	17.22	0.010	30.0	0.012	9.077	44.56	38.6%	0.4	0.9	5.4	73	-	0.2	24.1	At Flood Control Basin
TOTAL- Point 2				10.25				17.22													24.1	Peak Q at Tp = 24.1 min.
	1 1				1		1	1		1			1			1	1		-			
Drainage Area	Soil Group	Development	Area (sf)	Area (acre)	l (in/hr)	с	Q (ft ³ /s)	Q100 (ft ³ /s)	Slope	Section	Manning's (n)	Vf (ft/s)	Qf	Q/Qf	d/D	V/Vf	V (ft/s)	L (ft)	• H (ft)	T (min)	♦T (min)	Remarks
PR-3A	В	Apartment	13,490	0.31	3.32	0.8	0.82	0.82		-	-	-	-	-	-	-	-	215	6.7	6.8	6.8	Initial Area (Plate D-3)
PR-3B	В	Apartment	111,609	2.56	2.60	0.8	5.33	6.15	0.004	18.0	0.012	4.084	7.22	85.2%	0.7	1.1	3.2	737	-	3.8	10.6	
-	В	-	0	0.00	2.38	0	0.00	6.15	0.004	33.0	0.012	5.803	34.47	17.8%	0.3	0.7	3.7	389	-	1.8	12.4	At Flood Control Basin
					Adjust Q	to Tc = 2	4.1 min.															
TOTAL- Point 3				2.87	1		1	4.26			1 1				1	1	1			1	24.1	Peak Q at Tp = 24.1 min.

 ADJUSTMENTS TO POINT 1

 Adjust Te to TA =
 24.1
 min

 Qa =
 5.51
 cfs (Flow at Tc = 13.3 min)

 La =
 1.65
 in/frr (intensity at Tc = 24.1 min)

 La =
 2.29
 in/fr (intensity at Tc = 13.3 min)

 QADIUSTDE
 5.511 x (16.5 / 2.29)
 QADIUSTDE

ADJUSTMENTS TO POINT 3

Adjust TB to TA =	24.1	min	
QB =	6.15	cfs (Flow at Tc = 12.4 min)	
I_A =	1.65	in/hr (intensity at Tc = 24.1 min)	
Is =	2.38	in/hr (intensity at Tc = 12.4 min)	
QADJUSTED =	6.15 x (1.6	5 / 2.38)	
QADJUSTED =	4.26	cfs	
TOTAL DISCHAR	GE FRON	1 SITE = 3.97 + 17.22 + 4.26	
TOTAL POST-DE		25.45 CFS @ Tc = 24.1 MIN	

Appendix 3: Hydraulic Conditions of Concern Calculations

Unit Hydrograph Analysis

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Riverside County Synthetic Unit Hydrology Method RCFC & WCD Manual date - April 1978 Program License Serial Number 6538 _____ English (in-lb) Input Units Used English Rainfall Data (Inches) Input Values Used English Units used in output format _____ EXISTING POINT 1 ARLINGTON 03/15/2023 _____ Drainage Area = 6.92(Ac.) = 0.011 Sq. Mi. Drainage Area for Depth-Area Areal Adjustment = 6.92(Ac.) = 0.011 Sq. Mi. Length along longest watercourse = 1115.00(Ft.) Length along longest watercourse measured to centroid = 708.00(Ft.) Length along longest watercourse = 0.211 Mi. Length along longest watercourse measured to centroid = 0.134 Mi. Difference in elevation = 5.50(Ft.) Slope along watercourse = 26.0448 Ft./Mi. Average Manning's 'N' = 0.015 Lag time = 0.050 Hr. Lag time = 3.00 Min. 25% of lag time = 0.75 Min. 40% of lag time = 1.20 Min. Unit time = 5.00 Min. Duration of storm = 1 Hour(s) User Entered Base Flow = 0.00(CFS) 2 YEAR Area rainfall data: Area(Ac.)[1] Rainfall(In)[2] Weighting[1*2] 0.50 3.46 6.92 100 YEAR Area rainfall data: Area(Ac.)[1] Rainfall(In)[2] Weighting[1*2] 6.92 1.00 6.92

STORM EVENT (YEAR) = 2.00Area Averaged 2-Year Rainfall = 0.500(In) Area Averaged 100-Year Rainfall = 1.000(In) Point rain (area averaged) = 0.500(In) Areal adjustment factor = 99.99 % Adjusted average point rain = 0.500(In) Sub-Area Data: Area(Ac.) Runoff Index Impervious % 6.920 56.00 0.900 Total Area Entered = 6.92(Ac.) RI Infil. Rate Impervious Adj. Infil. Rate Area% RI F AMC2 AMC-2 (In/Hr) (Dec.%) (In/Hr) (Dec.) (In/Hr) 56.0 56.0 0.511 0.900 0.097 1.000 0.097 Sum(F) = 0.097Area averaged mean soil loss (F) (In/Hr) = 0.097Minimum soil loss rate ((In/Hr)) = 0.049 (for 24 hour storm duration) Soil low loss rate (decimal) = 0.180 _____ Slope of intensity-duration curve for a 1 hour storm =0.5500 _____ Unit Hydrograph VALLEY S-Curve _____ Unit Hydrograph Data Unit time period Time % of lag Distribution Unit Hydrograph Graph % (CFS) (hrs) 2.578 3.192 0.719 0.305 0.181 Sum = 100.000 Sum= 6.974 _____

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time	Pattern	Storm Rain	L	oss rate	(In./Hr)	Effective
	(Hr.)	Percent	(In/Hr)		Max	Low	(In/Hr)
1	0.08	3.30	0.198	(0.097)	0.036	0.162
2	0.17	4.20	0.252	(0.097)	0.045	0.207
3	0.25	4.40	0.264	(0.097)	0.048	0.216
4	0.33	4.80	0.288	(0.097)	0.052	0.236
5	0.42	5.20	0.312	(0.097)	0.056	0.256
6	0.50	6.20	0.372	(0.097)	0.067	0.305
7	0.58	6.80	0.408	(0.097)	0.073	0.335
8	0.67	8.80	0.528	(0.097)	0.095	0.433
9	0.75	13.90	0.834		0.097	(0.150)	0.737

31.40 1.884 10 0.83 0.097 (0.339) 1.787 (0.097) 11 0.92 7.20 0.432 0.078 0.354 3.80 (0.097) 12 1.00 0.228 0.041 0.187 (Loss Rate Not Used) Sum = 100.0 Sum = 5.2 Flood volume = Effective rainfall 0.43(In) times area 6.9(Ac.)/[(In)/(Ft.)] = 0.3(Ac.Ft) Total soil loss = 0.07(In) 0.038(Ac.Ft) Total soil loss = Total rainfall = 0.50(In) Flood volume = 10916.1 Cubic Feet 1642.9 Cubic Feet Total soil loss = _____ Peak flow rate of this hydrograph = 7.431(CFS) 1-HOUR STORM Runoff Hydrograph _____ Hydrograph in 5 Minute intervals ((CFS)) _____ Q(CFS) 0 2.5 Time(h+m) Volume Ac.Ft 5.0 7.5 10.0 _ _ _ _ _ _ _ _ _ _ _ _ _ _ _ _ _ _ _ 0+ 5 0.0029 0.42 VQ 0.0101 0+10 1.05 V Q 0+15 0.0193 1.33 νQ 0.0296 0+20 1.50 VQ 0+25 0.0411 1.66 Q 0+30 0.0540 1.88 QV 0+35 0.0687 2.13 0 V 2.53 3.66 0.0861 0+40 0 V 0+45 0.1113 3.66 0 V 7.43 V 0+50 0.1625 Q 0+55 0.2131 7.34 Q 1+ 0 0.2351 3.20 V Q 0.2456 1+ 5 1.53 Q 1+10 0.2495 0.57 0 0.2504 0.12 Q 1+15 V 0.2506 1+20 0.03 Q

Unit Hydrograph Analysis

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Riverside County Synthetic Unit Hydrology Method RCFC & WCD Manual date - April 1978 Program License Serial Number 6538 _____ English (in-lb) Input Units Used English Rainfall Data (Inches) Input Values Used English Units used in output format _____ EXISTING POINT 2 ARLINGTON 03/15/2023 _____ Drainage Area = 8.25(Ac.) = 0.013 Sq. Mi. Drainage Area for Depth-Area Areal Adjustment = 8.25(Ac.) = 0.013 Sq. Mi. Length along longest watercourse = 1770.00(Ft.) Length along longest watercourse measured to centroid = 730.00(Ft.) Length along longest watercourse = 0.335 Mi. Length along longest watercourse measured to centroid = 0.138 Mi. Difference in elevation = 5.50(Ft.) Slope along watercourse = 16.4068 Ft./Mi. Average Manning's 'N' = 0.015 Lag time = 0.066 Hr. Lag time = 3.95 Min. 25% of lag time = 0.99 Min. 40% of lag time = 1.58 Min. Unit time = 5.00 Min. Duration of storm = 1 Hour(s) User Entered Base Flow = 0.00(CFS) 2 YEAR Area rainfall data: Area(Ac.)[1] Rainfall(In)[2] Weighting[1*2] 0.50 4.13 8.25 100 YEAR Area rainfall data: Area(Ac.)[1] Rainfall(In)[2] Weighting[1*2] 8.25 1.00 8.25

STORM EVENT (YEAR) = 2.00Area Averaged 2-Year Rainfall = 0.500(In) Area Averaged 100-Year Rainfall = 1.000(In) Point rain (area averaged) = 0.500(In) Areal adjustment factor = 99.99 % Adjusted average point rain = 0.500(In) Sub-Area Data: Area(Ac.) Runoff Index Impervious % 8.250 56.00 0.900 Total Area Entered = 8.25(Ac.) RI Infil. Rate Impervious Adj. Infil. Rate Area% RI F AMC2 AMC-2 (In/Hr) (Dec.%) (In/Hr) (Dec.) (In/Hr) 56.0 56.0 0.511 0.900 0.097 1.000 0.097 Sum(F) = 0.097Area averaged mean soil loss (F) (In/Hr) = 0.097 Minimum soil loss rate ((In/Hr)) = 0.049 (for 24 hour storm duration) Soil low loss rate (decimal) = 0.180 _____ Slope of intensity-duration curve for a 1 hour storm =0.5500 _____ Unit Hydrograph VALLEY S-Curve _____ Unit Hydrograph Data Unit time period Time % of lag Distribution Unit Hydrograph Graph % (CFS) (hrs) _____

 1
 0.083
 126.555
 27.068

 2
 0.167
 253.110
 48.461

 3
 0.250
 379.666
 12.764

 4
 0.333
 506.221
 5.735

 5
 0.417
 632.776
 3.175

 6
 0.500
 759.331
 1.752

 7
 0.583
 885.886
 1.044

 2.251 4.029 1.061 0.477 0.264 0.146 0.087 Sum = 100.000 Sum= 8.314 _____

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time	Pattern	Storm Rain	Loss ra	Effective	
	(Hr.)	Percent	(In/Hr)	Max	Low	(In/Hr)
1	0.08	3.30	0.198	(0.097) 0.036	0.162
2	0.17	4.20	0.252	(0.097) 0.045	0.207
3	0.25	4.40	0.264	(0.097) 0.048	0.216
4	0.33	4.80	0.288	(0.097) 0.052	0.236
5	0.42	5.20	0.312	(0.097) 0.056	0.256
6	0.50	6.20	0.372	(0.097) 0.067	0.305
7	0.58	6.80	0.408	(0.097) 0.073	0.335

9 0.75 10 0.83 11 0.92	8.80 13.90 31.40 7.20 3.80 (Loss Ra ⁻	0.834 1.884 0.432 0.228	(0.097)	(0.095 0.150) 0.339) 0.078 0.041		737 787 354
tin Tota Tota Tota Floc Tota	•	fective 8.3(Ac. 0. 0.0 0.5 1301	rainfal)/[(In) 07(In) 45(Ac.F 0(In) 4.0 Cub 1958.6	/(Ft.)] t) ic Feet Cubic Fe	= et	0.3(Ac		
		1 - H u n o f graph in	I O U R f 5	S T C H y d r Minute i) R M o g r .nterv	aph als ((CFS	5))	
	0.0025	0.37 1.12 1.49 1.70 2.15 2.47 2.88 4.03 7.75 9.14 4.29 2.27 0.98 0.51 0.26 0.06	 VQ V Q V Q V Q		Q	 	 	

Unit Hydrograph Analysis

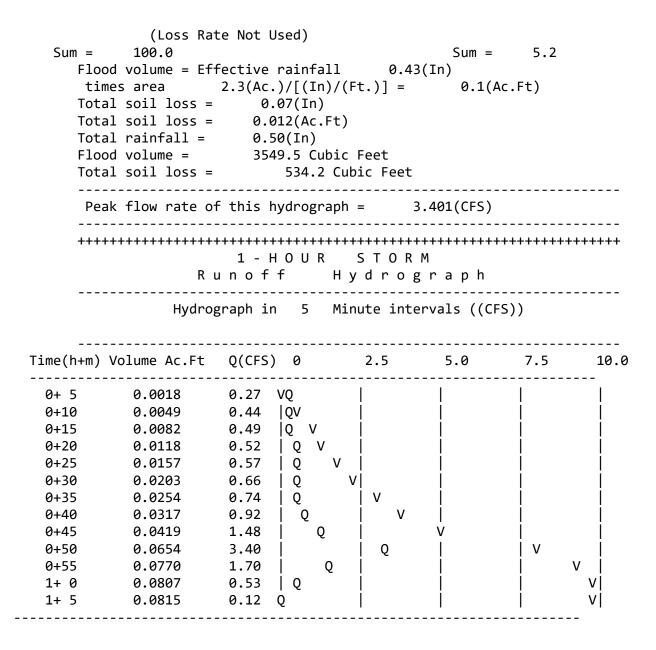
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Riverside County Synthetic Unit Hydrology Method RCFC & WCD Manual date - April 1978 Program License Serial Number 6538 _____ English (in-lb) Input Units Used English Rainfall Data (Inches) Input Values Used English Units used in output format EXISTING POINT 3 ARLINGTON 03/15/2023 _____ Drainage Area = 2.25(Ac.) = 0.004 Sq. Mi. Drainage Area for Depth-Area Areal Adjustment = 2.25(Ac.) = 0.004 Sq. Mi. Length along longest watercourse = 359.00(Ft.) Length along longest watercourse measured to centroid = 180.00(Ft.) Length along longest watercourse = 0.068 Mi. Length along longest watercourse measured to centroid = 0.034 Mi. Difference in elevation = 5.50(Ft.) Slope along watercourse = 80.8914 Ft./Mi. Average Manning's 'N' = 0.015 Lag time = 0.016 Hr. Lag time = 0.93 Min. 25% of lag time = 0.23 Min. 40% of lag time = 0.37 Min. Unit time = 5.00 Min. Duration of storm = 1 Hour(s) User Entered Base Flow = 0.00(CFS) 2 YEAR Area rainfall data: Area(Ac.)[1] Rainfall(In)[2] Weighting[1*2] 0.50 1.13 2.25 100 YEAR Area rainfall data: Area(Ac.)[1] Rainfall(In)[2] Weighting[1*2] 2.25 1.00 2.25

STORM EVENT (YEAR) = 2.00Area Averaged 2-Year Rainfall = 0.500(In) Area Averaged 100-Year Rainfall = 1.000(In) Point rain (area averaged) = 0.500(In) Areal adjustment factor = 100.00 % Adjusted average point rain = 0.500(In) Sub-Area Data: Area(Ac.) Runoff Index Impervious % 2.250 56.00 0.900 Total Area Entered = 2.25(Ac.) RI Infil. Rate Impervious Adj. Infil. Rate Area% RI F AMC2 AMC-2 (In/Hr) (Dec.%) (In/Hr) (Dec.) (In/Hr) 56.0 56.0 0.511 0.900 0.097 1.000 0.097 Sum(F) = 0.097Area averaged mean soil loss (F) (In/Hr) = 0.097 Minimum soil loss rate ((In/Hr)) = 0.049 (for 24 hour storm duration) Soil low loss rate (decimal) = 0.180 _____ Slope of intensity-duration curve for a 1 hour storm =0.5500 _____ Unit Hydrograph VALLEY S-Curve _____ Unit Hydrograph Data Unit time period Time % of lag Distribution Unit Hydrograph (hrs) Graph % (CFS) Graph % (CFS) 10.083534.90972.57220.1671069.81827.428 1.646 0.622 Sum = 100.000 Sum= 2.268 _____

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time	Pattern	Storm Rain	L	oss rate	(In.	/Hr)	Effective
	(Hr.)	Percent	(In/Hr)		Max	Lo	W	(In/Hr)
1	0.08	3.30	0.198	(0.097)		0.036	0.162
2	0.17	4.20	0.252	(0.097)		0.045	0.207
3	0.25	4.40	0.264	(0.097)		0.048	0.216
4	0.33	4.80	0.288	(0.097)		0.052	0.236
5	0.42	5.20	0.312	(0.097)		0.056	0.256
6	0.50	6.20	0.372	(0.097)		0.067	0.305
7	0.58	6.80	0.408	(0.097)		0.073	0.335
8	0.67	8.80	0.528	(0.097)		0.095	0.433
9	0.75	13.90	0.834		0.097	(0.150)	0.737
10	0.83	31.40	1.884		0.097	(0.339)	1.787
11	0.92	7.20	0.432	(0.097)		0.078	0.354
12	1.00	3.80	0.228	(0.097)		0.041	0.187



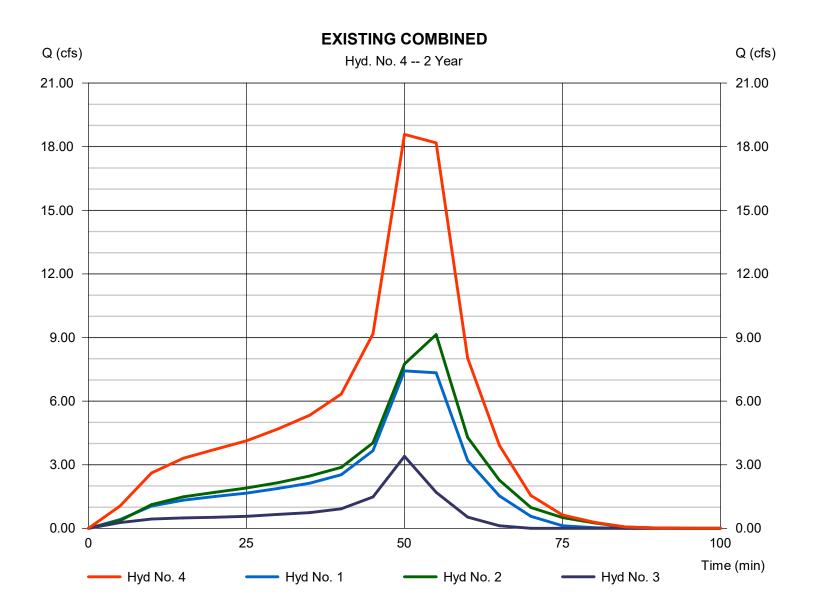
Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Hyd. No. 4

EXISTING COMBINED

Hydrograph type	= Combine	Peak discharge	= 18.58 cfs
Storm frequency	= 2 yrs	Time to peak	= 50 min
Time interval	= 5 min	Hyd. volume	= 27,483 cuft
Inflow hyds.	= 1, 2, 3	Contrib. drain. area	= 0.000 ac



Wednesday, 03 / 15 / 2023

Unit Hydrograph Analysis

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Riverside County Synthetic Unit Hydrology Method RCFC & WCD Manual date - April 1978 Program License Serial Number 6538 _____ English (in-lb) Input Units Used English Rainfall Data (Inches) Input Values Used English Units used in output format POST POINT 1 ARLINGTON 03/15/2023 _____ Drainage Area = 2.81(Ac.) = 0.004 Sq. Mi. Drainage Area for Depth-Area Areal Adjustment = 2.81(Ac.) = 0.004 Sq. Mi. Length along longest watercourse = 921.00(Ft.) Length along longest watercourse measured to centroid = 524.00(Ft.) Length along longest watercourse = 0.174 Mi. Length along longest watercourse measured to centroid = 0.099 Mi. Difference in elevation = 2.50(Ft.) Slope along watercourse = 14.3322 Ft./Mi. Average Manning's 'N' = 0.015 Lag time = 0.046 Hr. Lag time = 2.79 Min. 25% of lag time = 0.70 Min. 40% of lag time = 1.12 Min. Unit time = 5.00 Min. Duration of storm = 1 Hour(s) User Entered Base Flow = 0.00(CFS) 2 YEAR Area rainfall data: Area(Ac.)[1] Rainfall(In)[2] Weighting[1*2] 0.50 1.41 2.81 100 YEAR Area rainfall data: Area(Ac.)[1] Rainfall(In)[2] Weighting[1*2] 2.81 1.00 2.81

STORM EVENT (YEAR) = 2.00Area Averaged 2-Year Rainfall = 0.500(In) Area Averaged 100-Year Rainfall = 1.000(In) Point rain (area averaged) = 0.500(In) Areal adjustment factor = 100.00 % Adjusted average point rain = 0.500(In) Sub-Area Data: Area(Ac.) Runoff Index Impervious % 2.810 56.00 0.900 Total Area Entered = 2.81(Ac.) RI Infil. Rate Impervious Adj. Infil. Rate Area% RI F AMC2 AMC-2 (In/Hr) (Dec.%) (In/Hr) (Dec.) (In/Hr) 56.0 56.0 0.511 0.900 0.097 1.000 0.097 Sum(F) = 0.097Area averaged mean soil loss (F) (In/Hr) = 0.097Minimum soil loss rate ((In/Hr)) = 0.049 (for 24 hour storm duration) Soil low loss rate (decimal) = 0.180 _____ Slope of intensity-duration curve for a 1 hour storm =0.5500 _____ Unit Hydrograph VALLEY S-Curve _____ Unit Hydrograph Data Unit time period Time % of lag Distribution Unit Hydrograph Graph % (CFS) (hrs)

 1
 0.083
 179.330
 39.590

 2
 0.167
 358.660
 44.834

 3
 0.250
 537.990
 9.690

 4
 0.333
 717.320
 3.978

 5
 0.417
 896.651
 1.908

 1.121 1.270 0.274 0.113 0.054 Sum = 100.000 Sum= 2.832 _____

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time	Pattern	Storm Rain		Loss rate	(In./Hr)	Effective
	(Hr.)	Percent	(In/Hr)		Max	Low	(In/Hr)
1	0.08	3.30	0.198	(0.097)	0.036	0.162
2	0.17	4.20	0.252	(0.097)	0.045	0.207
3	0.25	4.40	0.264	(0.097)	0.048	0.216
4	0.33	4.80	0.288	(0.097)	0.052	0.236
5	0.42	5.20	0.312	(0.097)	0.056	0.256
6	0.50	6.20	0.372	(0.097)	0.067	0.305
7	0.58	6.80	0.408	(0.097)	0.073	0.335
8	0.67	8.80	0.528	(0.097)	0.095	0.433
9	0.75	13.90	0.834		0.097	(0.150)	0.737

10 0.83 31.40 1.884 0.097 (0.339) 1.787 (0.097) 11 0.92 7.20 0.432 0.078 0.354 3.80 0.228 (0.097) 0.187 12 1.00 0.041 (Loss Rate Not Used) Sum = 100.0 Sum = 5.2 Flood volume = Effective rainfall 0.43(In) times area 2.8(Ac.)/[(In)/(Ft.)] = 0.1(Ac.Ft) Total soil loss = 0.07(In) 0.015(Ac.Ft) Total soil loss = Total rainfall = 0.50(In) 4432.9 Cubic Feet Flood volume = 667.1 Cubic Feet Total soil loss = -----_ _ _ _ _ _ _ _ _ _ _ _ _ _ _ _ _ _ _ Peak flow rate of this hydrograph = 3.114(CFS) 1-HOUR STORM Runoff Hydrograph _____ Hydrograph in 5 Minute intervals ((CFS)) Time(h+m) Volume Ac.Ft Q(CFS) 0 2.5 5.0 7.5 10.0 ------_ _ _ _ _ _ _ _ _ _ _ _ _ _ _ _ 0+ 5 0.0013 0.18 Q 0.0043 0.44 Q 0+10 0+15 0.0081 0.55 | QV 0.0123 0+20 0.61 ΙQV 0.68 Q V 0+25 0.0170 0+30 0.0223 0.77 | Q V | 0+35 0.0283 0.87 | Q IV 0.0354 0.0458 1.04 | Q 0+40 V 0+45 1.52 V Q 3.11 0+50 0.0673 Q V 0+55 0.0875 2.94 Q 1.26 1+ 0 0.0962 ٧ Q 0.1001 1+ 5 0.58 | Q 1+10 0.1014 0.19 Q 0.04 Q 1+15 0.1017 V 1+20 0.1018 0.01 Q

Unit Hydrograph Analysis

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Riverside County Synthetic Unit Hydrology Method RCFC & WCD Manual date - April 1978 Program License Serial Number 6538 _____ English (in-lb) Input Units Used English Rainfall Data (Inches) Input Values Used English Units used in output format POST POINT 2 ARLINGTON 03/15/2023 _____ Drainage Area = 9.58(Ac.) = 0.015 Sq. Mi. Drainage Area for Depth-Area Areal Adjustment = 9.58(Ac.) = 0.015 Sq. Mi. Length along longest watercourse = 1796.00(Ft.) Length along longest watercourse measured to centroid = 898.00(Ft.) Length along longest watercourse = 0.340 Mi. Length along longest watercourse measured to centroid = 0.170 Mi. Difference in elevation = 4.00(Ft.) Slope along watercourse = 11.7595 Ft./Mi. Average Manning's 'N' = 0.015Lag time = 0.076 Hr. Lag time = 4.58 Min. 25% of lag time = 1.14 Min. 40% of lag time = 1.83 Min. Unit time = 5.00 Min. Duration of storm = 1 Hour(s) User Entered Base Flow = 0.00(CFS) 2 YEAR Area rainfall data: Area(Ac.)[1] Rainfall(In)[2] Weighting[1*2] 0.50 4.79 9.58 100 YEAR Area rainfall data: Area(Ac.)[1] Rainfall(In)[2] Weighting[1*2] 9.58 1.00 9.58

STORM EVENT (YEAR) = 2.00Area Averaged 2-Year Rainfall = 0.500(In) Area Averaged 100-Year Rainfall = 1.000(In) Point rain (area averaged) = 0.500(In) Areal adjustment factor = 99.99 % Adjusted average point rain = 0.500(In) Sub-Area Data: Area(Ac.) Runoff Index Impervious % 9.580 56.00 0.900 Total Area Entered = 9.58(Ac.) RI Infil. Rate Impervious Adj. Infil. Rate Area% RI F AMC2 AMC-2 (In/Hr) (Dec.%) (In/Hr) (Dec.) (In/Hr) 56.0 56.0 0.511 0.900 0.097 1.000 0.097 Sum(F) = 0.097Area averaged mean soil loss (F) (In/Hr) = 0.097Minimum soil loss rate ((In/Hr)) = 0.049 (for 24 hour storm duration) Soil low loss rate (decimal) = 0.180 _____ Slope of intensity-duration curve for a 1 hour storm =0.5500 _____ Unit Hydrograph VALLEY S-Curve _____ Unit Hydrograph Data Unit time period Time % of lag Distribution Unit Hydrograph Graph % (CFS) (hrs) _____ 2.124 4.714 1.390 0.636 0.353 0.221 0.130 0.087 Sum = 100.000 Sum= 9.655 _____

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time	Pattern	Storm Rain	Loss rate	Effective	
	(Hr.)	Percent	(In/Hr)	Max	Low	(In/Hr)
1	0.08	3.30	0.198	(0.097)	0.036	0.162
2	0.17	4.20	0.252	(0.097)	0.045	0.207
3	0.25	4.40	0.264	(0.097)	0.048	0.216
4	0.33	4.80	0.288	(0.097)	0.052	0.236
5	0.42	5.20	0.312	(0.097)	0.056	0.256
6	0.50	6.20	0.372	(0.097)	0.067	0.305

(0.097) 0.58 6.80 0.408 0.073 7 0.335 (0.097) 8 0.67 8.80 0.528 0.095 0.433 (0.150) 9 0.75 13.90 0.834 0.097 0.737 0.097 10 0.83 31.40 1.884 (0.339) 1.787 0.432 7.20 (0.097) 11 0.92 0.078 0.354 3.80 12 1.00 0.228 (0.097) 0.041 0.187 (Loss Rate Not Used) Sum = 100.0 Sum = 5.2 Flood volume = Effective rainfall 0.43(In) 9.6(Ac.)/[(In)/(Ft.)] = times area 0.3(Ac.Ft) Total soil loss = 0.07(In) Total soil loss = 0.052(Ac.Ft) Total rainfall = 0.50(In) Flood volume = 15111.8 Cubic Feet Total soil loss = 2274.3 Cubic Feet -----Peak flow rate of this hydrograph = 10.719(CFS) _____ 1 - HOUR STORM Runoff Hydrograph -----Hydrograph in 5 Minute intervals ((CFS)) _____ Time(h+m) Volume Ac.Ft Q(CFS) 0 5.0 10.0 15.0 20.0 _____ 0+ 5 0.0024 0.34 Q 1.20 VQ 0+10 0.0107 0+15 0.0221 1.66 | VQ 0+20 0.0353 1.91 l ov 0+25 0.0501 2.15 0V Q V I 0+30 0.0668 2.43 2.80 Q V 0+35 0.0861 Q 0+40 0.1085 3.26 l v 4.46 0+45 0.1392 Q V 8.30 0.1964 0+50 Q V 0+55 0.2702 10.72 0 I٧ 1+ 0 5.31 0.3068 0 1+ 5 0.3270 2.94 Q v 1+10 0.3364 1.37 Q V 1+15 0.3417 0.77 Q 0.44 Q 1+20 0.3448 V 0.24 Q 1+25 0.3464 v 1+30 0.3468 0.06 Q 0.3469 0.02 Q 1+35 _ _ _ _ _ _ _ _ _ _

Unit Hydrograph Analysis

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Riverside County Synthetic Unit Hydrology Method RCFC & WCD Manual date - April 1978 Program License Serial Number 6538 _____ English (in-lb) Input Units Used English Rainfall Data (Inches) Input Values Used English Units used in output format POST POINT 3 ARLINGTON 03/15/2023 _____ Drainage Area = 2.87(Ac.) = 0.004 Sq. Mi. Drainage Area for Depth-Area Areal Adjustment = 2.87(Ac.) = 0.004 Sq. Mi. Length along longest watercourse = 952.00(Ft.) Length along longest watercourse measured to centroid = 476.00(Ft.) Length along longest watercourse = 0.180 Mi. Length along longest watercourse measured to centroid = 0.090 Mi. Difference in elevation = 12.00(Ft.) Slope along watercourse = 66.5546 Ft./Mi. Average Manning's 'N' = 0.015Lag time = 0.034 Hr. Lag time = 2.03 Min. 25% of lag time = 0.51 Min. 40% of lag time = 0.81 Min. Unit time = 5.00 Min. Duration of storm = 1 Hour(s) User Entered Base Flow = 0.00(CFS) 2 YEAR Area rainfall data: Area(Ac.)[1] Rainfall(In)[2] Weighting[1*2] 0.50 1.44 2.87 100 YEAR Area rainfall data: Area(Ac.)[1] Rainfall(In)[2] Weighting[1*2] 2.87 1.00 2.87

STORM EVENT (YEAR) = 2.00Area Averaged 2-Year Rainfall = 0.500(In) Area Averaged 100-Year Rainfall = 1.000(In) Point rain (area averaged) = 0.500(In) Areal adjustment factor = 100.00 % Adjusted average point rain = 0.500(In) Sub-Area Data: Area(Ac.) Runoff Index Impervious % 2.870 56.00 0.900 Total Area Entered = 2.87(Ac.) RI Infil. Rate Impervious Adj. Infil. Rate Area% RI F AMC2 AMC-2 (In/Hr) (Dec.%) (In/Hr) (Dec.) (In/Hr) 56.0 56.0 0.511 0.900 0.097 1.000 0.097 Sum(F) = 0.097Area averaged mean soil loss (F) (In/Hr) = 0.097Minimum soil loss rate ((In/Hr)) = 0.049 (for 24 hour storm duration) Soil low loss rate (decimal) = 0.180 -----Slope of intensity-duration curve for a 1 hour storm =0.5500 _____ Unit Hydrograph VALLEY S-Curve _____ Unit Hydrograph Data Unit time period Time % of lag Distribution Unit Hydrograph Graph % (CFS) (hrs) 10.083245.89550.35520.167491.78940.30930.250737.6847.15640.333983.5792.180 1.456 1.166 0.207 0.063 Sum = 100.000 Sum= 2.892 _____

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	: Time	Pattern	Storm Rain	Loss rate(In./Hr)		Effective		
	(Hr.)	Percent	(In/Hr)	М	lax	Lo	W	(In/Hr)
1	0.08	3.30	0.198	(0.097)		0.036	0.162
2	0.17	4.20	0.252	(0.097)		0.045	0.207
3	0.25	4.40	0.264	(0.097)		0.048	0.216
4	0.33	4.80	0.288	(0.097)		0.052	0.236
5	0.42	5.20	0.312	(0.097)		0.056	0.256
6	0.50	6.20	0.372	(0.097)		0.067	0.305
7	0.58	6.80	0.408	(0.097)		0.073	0.335
8	0.67	8.80	0.528	(0.097)		0.095	0.433
9	0.75	13.90	0.834		0.097	(0.150)	0.737
10	0.83	31.40	1.884		0.097	(0.339)	1.787

0.92 7.20 (0.097) 0.078 11 0.432 0.354 12 1.00 0.228 (0.097) 0.041 3.80 0.187 (Loss Rate Not Used) Sum = Sum = 100.0 5.2 Flood volume = Effective rainfall 0.43(In) times area 2.9(Ac.)/[(In)/(Ft.)] = 0.1(Ac.Ft) Total soil loss = 0.07(In) Total soil loss = 0.016(Ac.Ft) 0.50(In) Total rainfall = Flood volume = 4527.5 Cubic Feet Total soil loss = 681.4 Cubic Feet _____ Peak flow rate of this hydrograph = 3.574(CFS) _____ 1-HOUR STORM Runoff Hydrograph Hydrograph in 5 Minute intervals ((CFS)) _____ Q(CFS) 0 2.5 Time(h+m) Volume Ac.Ft 10.0 5.0 7.5 -----0+ 5 0.0016 0.24 0 0.0050 0.49 Q 0+10 0+15 0.0091 0.59 QV 0+20 0.0135 0.65 | Q V 0+25 0.0184 0.71 | Q V 0+30 0.0240 0.81 Q 0+35 0.0302 0.91 Q 0+40 0.0378 1.10 0 V 0.0493 0+45 1.67 0 V 0+50 0.0739 3.57 V Q 2.78 0+55 0.0931 Q V 1+ 0 0.1007 1.10 | Q v 1+ 5 0.1034 0.40 Q 0.1039 1+10 0.06 Q 1+15 0.1039 0.01 Q

Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Wednesday, 03 / 15 / 2023

Hyd. No. 4

POST COMBINED

Hydrograph type	 = Combine = 2 yrs = 5 min = 1, 2, 3 	Peak discharge	= 16.44 cfs
Storm frequency		Time to peak	= 55 min
Time interval		Hyd. volume	= 24,078 cuft
Inflow hyds.		Contrib. drain. area	= 0.000 ac
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